

# Spectroscopic immersion ellipsometry study of the mechanism of Si/SiO<sub>2</sub> interface annealing

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In this study we apply an interface sensitive ellipsometry technique to study the evolution of the Si-SiO<sub>2</sub> interface as a function of high temperature annealing (750–1100 °C). Essentially, the ellipsometry technique embodies the use of liquids that refractive index match with the bulk film thereby removing the optical response of the overlayer and greatly enhancing sensitivity to the interface. According to both time and temperature of anneal, distinct modes of behavior are observed for the evolution of the interface. For short anneal times a rapid change in the interface is observed that correlates with the disappearance of protrusions, followed by a slower change that correlates with the disappearance of the suboxide. At high temperatures viscous relaxation dominates, while at low temperatures the suboxide reduction is apparent. A model for the interface in terms of chemical and physical interface processes is proposed and model parameters are compared with literature results.

## I. INTRODUCTION

The Si/SiO<sub>2</sub> interface continues to be a topic of intensive study. Of particular importance are properties of the interface such as structure, thickness, uniformity, and phase composition which have been explored by numerous methods including transmission electron microscopy (TEM),<sup>1–2</sup> infrared spectroscopy (IRS),<sup>3</sup> low-energy electron diffraction (LEED),<sup>4</sup> scanning tunneling microscopy (STM),<sup>5</sup> ellipsometry,<sup>6–10</sup> and a variety of surface spectroscopies.<sup>11</sup> Presently, ultrathin SiO<sub>2</sub> films (thickness less than 30 nm) find extensive application in submicron integrated circuit technology where even a small degree of interfacial micro-roughness or nonuniformity can alter device performance and reliability. In order to improve interfacial quality, such processing procedures as two-step oxidation process<sup>12,13</sup> and postoxidation annealing<sup>14,15</sup> have been proposed. Both methods include annealing of the grown oxides in a non-oxidizing atmosphere such as argon or nitrogen. High-resolution TEM was used to investigate the influence of the annealing on interface smoothness,<sup>12,13,16</sup> but the results are ambiguous and on some points contradictory. Yet there seems to be general agreement that annealing improves both electronic properties and interface flatness.

Spectroscopic ellipsometry has been applied to study interfaces under transparent films,<sup>17</sup> and recently we reported an interface enhanced immersion spectroscopic technique,<sup>18</sup> which is sensitive to such interface characteristics as microroughness, thickness, and phase composition. In the present study, we apply this new method to determine the properties and reactions at the Si/SiO<sub>2</sub> interface during the postoxidation annealing.

## II. EXPERIMENTAL PROCEDURES AND DATA ANALYSIS

Single-crystal (100) oriented 2 Ω cm *p*-type silicon wafers were cleaned using a slightly modified RCA procedure<sup>19</sup> and thermally oxidized in a fused silica tube

furnace in clean dry oxygen to about 24–27 nm SiO<sub>2</sub> at 800 °C. Upon completion of a particular oxidation one sample was removed without annealing as a control, and the others were annealed in a clean nitrogen atmosphere. We used annealing temperatures and times in the range 750–1100 °C and 1–120 min, respectively.

In order to investigate the Si/SiO<sub>2</sub> interface, we have applied a novel enhanced sensitivity spectral and variable angle of incidence immersion ellipsometry technique.<sup>18</sup> The key feature of this technique is that spectroscopic and variable angle of incidence ellipsometry measurements are performed with the sample in a transparent liquid ambient that has optical properties very close to those of the SiO<sub>2</sub> overlayer. Therefore, the overlayer film is “optically” (not physically) eliminated, and the probing light beam becomes highly sensitive to the interface properties.

Generally, it is difficult to achieve a perfect refractive index match for the liquid ambient  $n_0$ , and the SiO<sub>2</sub> overlayer  $n_{ov}$ , over a broad spectral range. Therefore deviations are accounted for in the analysis.<sup>18</sup>

Carbon tetrachloride (CCl<sub>4</sub>) is a suitable immersion liquid for matching index to SiO<sub>2</sub> films. The refractive index of the liquid ambient  $n_0$  was calculated from a Cauchy dispersion formula, taking into account temperature:

$$n_0 = n_\infty + \frac{a}{\lambda^2} + \frac{\partial n}{\partial T} \Delta T, \quad (1)$$

where  $\lambda$  in angstroms is the wavelength of probing beam, parameters  $n_\infty = 1.4427$ ,  $a = 5.15 \times 10^5 \text{ Å}^{-2}$  at  $T = 24.8 \text{ °C}$ ,<sup>20</sup> and  $\partial n / \partial T = 0.00055$  at  $T = 20 \text{ °C}$  for pure CCl<sub>4</sub>.<sup>21</sup>

It is known that the refractive index of thin-film SiO<sub>2</sub> overlayers  $n_{ov}$  depends on thickness  $L_{ov}$ , oxidation temperature  $T_{ox}$ , annealing temperature  $T_{an}$ , and time  $t_{an}$ , index of the substrate orientation  $N$ , and preparation conditions such as preoxidation cleaning and oxidation ambient. The spectral dependence of the nonannealed thin-film SiO<sub>2</sub> re-

fractive index,  $n_{ov}^0(L_{ov}, T_{ox}, \lambda)$ , for a substrate with particular orientation, e.g., (100), was calculated from a single term Sellmeier approximation as follows:

$$n_{ov}^0(L_{ov}, T_{ox}, N, \lambda) = 1 + \frac{A(L_{ov}, T_{ox}, N)\lambda^2}{\lambda^2 - \lambda_0^2(L_{ov}, T_{ox}, N)}, \quad (2)$$

where  $A(L_{ov}, T_{ox}, N)$  and  $\lambda_0(L_{ov}, T_{ox}, N)$  are dispersion parameters that are also dependent on the overlayer thickness and preparation conditions and with values  $A = 1.15$  and  $\lambda_0 = 92.3$  nm for 25–35 nm thick SiO<sub>2</sub> films thermally grown at 800 °C on Si(100).<sup>10</sup>

It has been observed that the refractive index of the SiO<sub>2</sub> overlayer undergoes a relaxation during annealing.<sup>22–25</sup> Ellipsometric measurements of the thermal relaxation of the SiO<sub>2</sub> single film effective refractive index, i.e., without taking the interface into consideration, shows<sup>23</sup> that two relaxation processes are involved: rapid (~1–2 min) initial relaxation and slow exponential decay to the refractive index of fully relaxed oxide. The slow exponential decay is because of the elastic strain relaxation and well described as

$$n_{ov}(L_{ov}, T_{ox}, T_{an}, t_{an}, N, \lambda) = n_f(\lambda) + [n_{ov}^0(\lambda) - n_f(\lambda)] \times \exp\left(-\frac{t_{an}}{\tau}\right)^\eta, \quad (3)$$

where  $n_f$  is the refractive index for fully relaxed oxide, and the empirical parameter  $\eta = 0.17$ ,<sup>22</sup> which is a measure of the strength of the coupling between the index and relaxation. The relaxation time for the oxide density is expressed as

$$\tau(T_{an}) = \tau_0 \exp\left(\frac{E_0}{kT_{an}}\right), \quad (4)$$

where  $\tau_0 \sim 2 \times 10^{-23}$  min and  $E_0 \sim 6$  eV.<sup>22</sup> We have assumed that the refractive index of the fully relaxed oxide film is equal to that for bulk vitreous oxide, and thus the spectral dependence  $n_f(\lambda)$  was calculated with Eq. (2) using  $A = 1.099$  and  $\lambda_0 = 92.27$ <sup>10</sup> which corresponds to vitreous SiO<sub>2</sub>. The observed initial rapid relaxation of the effective refractive index<sup>23</sup> can be attributed to the evolution of the interface, and a detailed model for this will be discussed below.

In order to obtain unknown interface parameters, we used a Marquardt nonlinear best fit algorithm which minimizes the value of the error function

$$Q = \sum_{ij} [(\Delta_{ij}^{cal}(\phi_i, E_j, P) - \Delta_{ij}^{exp})^2 + (\Psi_{ij}^{cal}(\phi_i, E_j, P) - \Psi_{ij}^{exp})^2], \quad (5)$$

where  $P$  is a vector of unknown interface parameters,  $E_j$  is the photon energy,  $\phi_i$  is the angle of incidence, and the subscripts cal and exp refer to calculated and experimentally derived values.  $\Delta^{cal}$  and  $\Psi^{cal}$  are the values obtained using the vector  $P$  from expanded Fresnel formulas,<sup>26</sup> and a matrix algorithm for the multilayer system with optical parameters for the CCl<sub>4</sub> ambient and SiO<sub>2</sub> overlayer calculated from the Eqs. (1)–(4), and the previously deter-

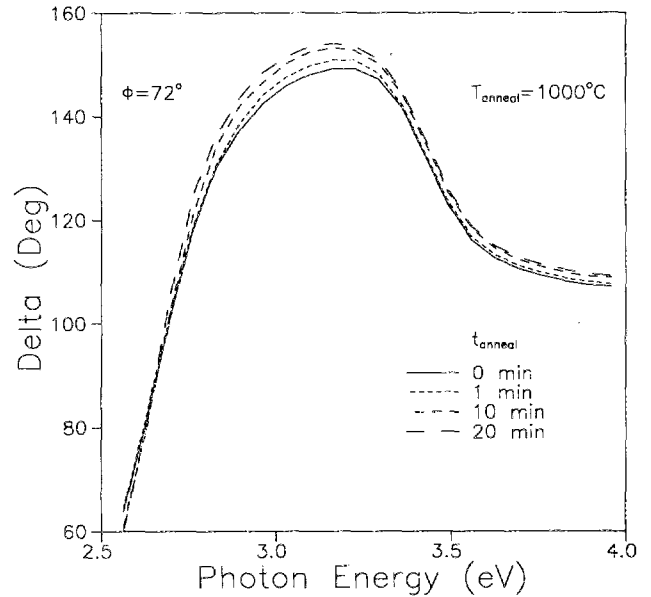


FIG. 1. The experimental dependence of the ellipsometric angle  $\Delta$  on photon energy  $E$  at different annealing times.

mined thickness of the SiO<sub>2</sub> overlayer. The Bruggeman effective medium approximation (BEMA),<sup>27</sup> was used to calculate the effective dielectric function of the interface, which was modeled as a mixture of constituents (discussed later) with known optical properties. Volume fractions of the constituents were calculated from assumptions about the geometry of the interface that are discussed below, and the geometrical parameters have been included as unknown parameters.

A commercially available vertical ellipsometer bench was modified to become a rotating analyzer spectroscopic ellipsometer (the essential features were previously described<sup>28</sup>) and calibrated according to a published procedure.<sup>29</sup> A specially designed variable angle of incidence immersion cell that fits on the ellipsometer stage was used.<sup>18</sup> For each sample spectroscopic ellipsometry was performed both in air and CCl<sub>4</sub> in the 2.4–4.0 eV range of photon energies  $E$  and at two angles of incidence  $\phi$  of 72° and 75°. The measurements yield the ellipsometric angles  $\Delta^{exp}(E, \phi, T_{an}, t_{an})$  (Fig. 1) and  $\Psi^{exp}(E, \phi, T_{an}, t_{an})$  as a function of annealing conditions ( $T_{an}, t_{an}$ ). As was previously discussed,<sup>18</sup> the sensitivity of  $\Psi$  to interface changes is considerably less than for  $\Delta$ , hence only  $\Delta$  is used to correlate with process changes. From the measurements done in air, the thickness of the SiO<sub>2</sub> overlayer was obtained without significant error, because there is very low interface sensitivity for the measurements in air.<sup>18</sup>

In order to obtain interface dependencies, which characterize the evolution of the interface via annealing, we have calculated an effective relative interface parameter

$$\delta\Delta_{int}(T_{an}, t_{an}) = \Delta^{exp}(T_{an}, t_{an}) - \Delta_0^{exp} - \delta\Delta_{ov}^{cal}(T_{an}, t_{an}), \quad (6)$$

where  $\Delta^{exp}(T_{an}, t_{an})$  is the experimental ellipsometric angle  $\Delta$  at an annealing temperature and time,  $\Delta_0$  is the ellipso-

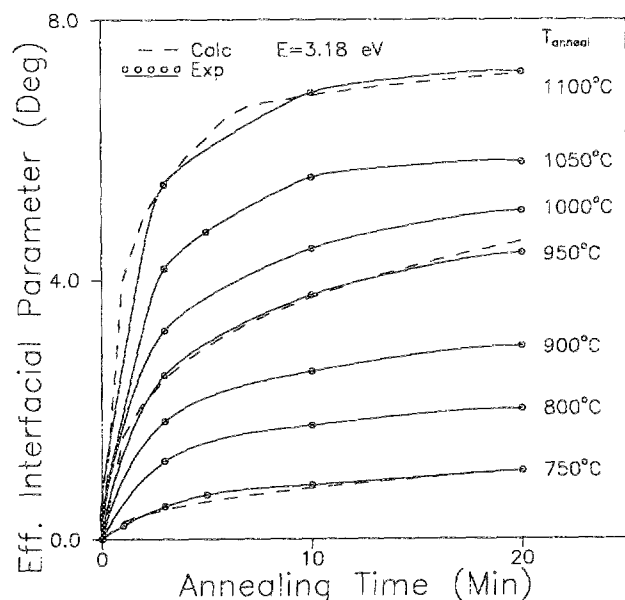


FIG. 2. The experimental dependence of the effective interface parameter  $\Delta_{\text{inf}}$  on annealing time at a number of annealing temperatures. A simulated dependency is shown with the dashed curve.

metric angle for a nonannealed sample and the term  $\delta\Delta_{\text{ov}}^{\text{cal}}(T_{\text{an}}, t_{\text{an}})$  is the overlayer relaxation correction. This correction term represents the difference in  $\Delta$  for the single-film (without interface) system of a nonannealed and annealed overlayer with the refractive index calculated from Eqs. (2)–(4); and this correction represents only a few percent of  $\delta\Delta_{\text{inf}}$ . The chosen photon energy  $E = 3.18$  eV is in the range of the maximum interface and the minimum overlayer sensitivity.<sup>18</sup>

### III. RESULTS AND DISCUSSION

#### A. Model independent results

First, Fig. 1 shows that  $\Delta^{\text{exp}}(E, \phi, T_{\text{an}}, t_{\text{an}})$  is measured with enhanced sensitivity at different annealing conditions in the spectral energy range 2.8–3.4 eV. Figures 2 and 3 display experimental results in terms of the interface parameter  $\delta\Delta_{\text{inf}}(T_{\text{an}}, t_{\text{an}})$  defined by Eq. (6) above. Thus, Figs. 2 and 3 show the values for  $\delta\Delta_{\text{inf}}$  measured at 3.18 eV versus anneal time at a number of temperatures in Fig. 2 and versus anneal temperature at two times in Fig. 3. Other information relating to modelling is also included in Fig. 3, but discussion of these items will be deferred to later sections. It is seen in Fig. 2 that at all annealing temperatures two temporal regions of behavior are present. Initially, the anneals yield a fast increase in  $\delta\Delta_{\text{inf}}$  that slows quickly after 5 min and then nearly saturates. Taking the data from Fig. 2 at two anneal times, one before and one near saturation, and plotting versus anneal temperature reveals a distinct break in the 900–970 °C range, which corresponds to the viscous flow range, i.e., a temperature above which viscous flow of the oxide is fast.<sup>30</sup> Thus, we consider that the viscous relaxation dominates at the higher anneal temperatures, but at lower temperatures we need to consider other possible mechanisms. It is clear that

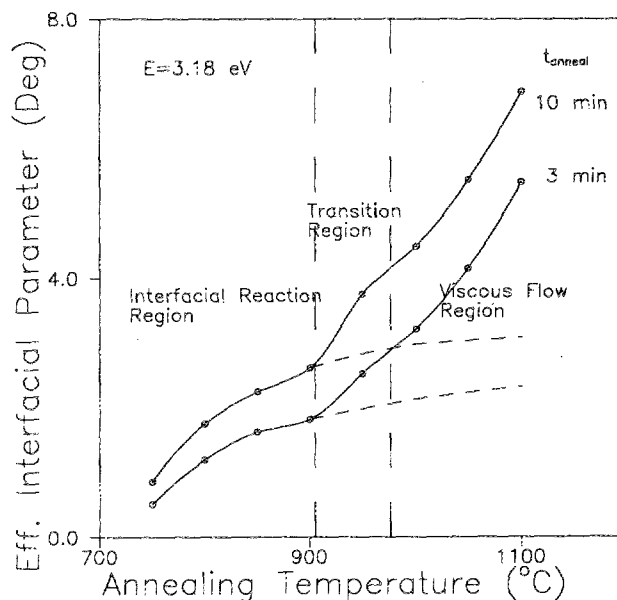


FIG. 3. The experimental dependence of the effective interface parameter  $\Delta_{\text{inf}}$  on annealing temperature for two annealing times.

the low temperature mechanism accounts for a large part of the change in  $\delta\Delta_{\text{inf}}$ .

If the interface region is treated as a single homogenous film, then the extent of the interface is observed to decrease with both annealing time and temperature as evidenced by the increasing  $\Delta_{\text{inf}}$ . With both a decrease in the interface region for short and long times and low and high temperatures the models that are chosen for the different modes of behavior must show the same characteristics.

#### B. Working model for the Si-SiO<sub>2</sub> interface

The transition from crystalline Si, *c*-Si, to bulk amorphous SiO<sub>2</sub> includes at least two physically distinct regions. First there is a short range decay region from the *c*-Si in which the long-range crystalline order of *c*-Si disappears, i.e., the memory of the Si order is lost. The characteristic range for this zone is 0.1–2 nm. Second, there is a longer range decay region possibly extending to tens of nanometers into the amorphous SiO<sub>2</sub> film where mechanical stress, density, and refractive index relax to the bulk SiO<sub>2</sub> film values. Annealing decreases the extent of both regions. One way to think about the interface between film and substrate is as a transition region that has a structure with two major components each with a substructure: the “physical” interface and the “chemical” interface. The “physical” interface consists of a mixture of substrate and overlayer constituents, which can represent microroughness or protrusions of Si into the oxide and even inclusions of SiO<sub>2</sub> microcrystallites, such as cristobalite or tridymite.<sup>10</sup> This layer represents an order transition. The “chemical” interface consists of a new chemical compound with a wide homogeneity range, a suboxide, SiO<sub>*x*</sub>, with  $0 < x < 2$ . In the chemical interface we permit other properties such as stress, density, and refractive index (which are likely related)<sup>24</sup> to relax to bulk values.

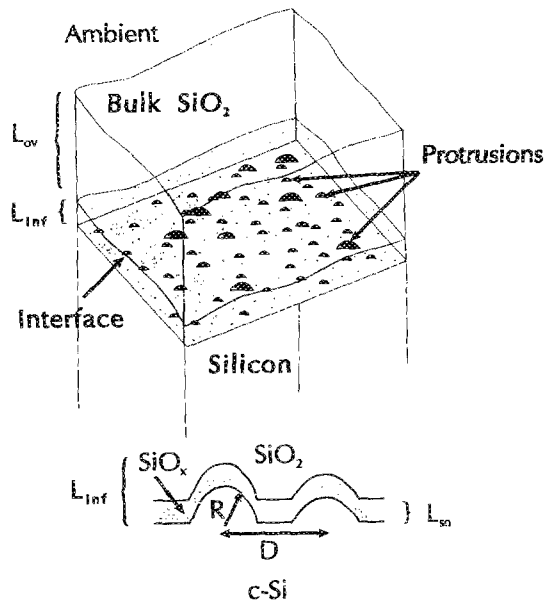


FIG. 4. Schematic representation of our interface model.

For the purpose of analyzing the experimental data in terms of physical parameters, we propose a model for the interface consisting of these two distinct entities: the physical and chemical interfaces. The physical interface is modeled as Si protrusions whose distribution and size are important parameters. The chemical interface is modeled as a suboxide that coats the physical interface, and lies between the Si surface with protrusions and the overlayer SiO<sub>2</sub>. Figure 4 shows a sketch of our model; the cross section displays parameters defined further below. Below we provide the parameters that quantify this working model, and then the experimental data  $\Delta^{\text{exp}}(E, \phi, T_{\text{an}}, t_{\text{an}})$ ,  $\psi^{\text{exp}}(E, \phi, T_{\text{an}}, t_{\text{an}})$  from Figs. 2 and 3 are reduced to yield values for the model parameters which are compared with other studies about the interface region. Finally, we discuss the mechanisms that could diminish both interfaces with annealing, since that is what we observe. It should be understood that our model is a "working" model based on many presently available research results. While we show good agreement between the parameters obtained in this model and independent measurements on the interface region, we do not prove our model but only further demonstrate its reasonableness, and more importantly provide physically relevant parameter changes related to the condition of the interface such as surface roughness and stoichiometry.

We describe the crystalline silicon protrusions as hemispheres with an average radius  $R$ , which form a hexagonal network with an average distance  $D$  between centers of the protrusions. Thus the protrusions define the "physical" interface with a thickness  $R$ . The protrusions and the region between them are covered by a layer of suboxide SiO<sub>*x*</sub>,  $0 < x < 2$ , with an average thickness  $L_{\text{so}}$ . This layer forms a chemical transition zone from Si to SiO<sub>2</sub> or the "chemical" interface. It is possible to model both the "physical" and

the "chemical" interfaces as one transition layer with an effective thickness:

$$L_{\text{inf}} = R + L_{\text{so}}, \quad (7)$$

and an effective dielectric function  $\epsilon_{\text{inf}}$ , which represents a mixture of crystalline silicon *c*-Si, silicon suboxide SiO<sub>*x*</sub> and the SiO<sub>2</sub> overlayer and written as:

$$\epsilon_{\text{inf}} = \epsilon_{\text{inf}}(\epsilon_{\text{c-Si}} f_{\text{c-Si}} \epsilon_{\text{SiO}_x} f_{\text{SiO}_x} \epsilon_{\text{SiO}_2} f_{\text{SiO}_2}) \quad (8)$$

$\epsilon_{\text{inf}}$  was calculated using the BEMA, where the dielectric properties  $\epsilon$ , and relative volume fractions  $f$  of all of the interfacial layer constituents are known a priori. The dielectric function of SiO<sub>*x*</sub> was calculated using the BEMA, and by considering that SiO<sub>*x*</sub> is a mixture of amorphous silicon, *a*-Si, and SiO<sub>2</sub>.<sup>31</sup> The relative volume fractions of Si-Si and Si-O bonds,  $f_{\text{Si-Si}}$  and  $f_{\text{Si-O}}$ , respectively, are as follows; The refractive index of the SiO<sub>2</sub> overlayer was calculated from

$$f_{\text{Si-Si}} = \frac{2-x}{2+x}, \quad f_{\text{Si-O}} = \frac{2x}{2+x} \quad (9)$$

Eqs. (2)–(4). The relative volume fractions of the interfacial layer constituents  $f_{\text{c-Si}}$ ,  $f_{\text{SiO}_x}$ , and  $f_{\text{SiO}_2}$  were calculated from the assumed geometry of the interface and given as:

$$f_{\text{c-Si}} = \frac{4\pi R \rho^2}{3\sqrt{3}(R + L_{\text{so}})}, \quad \rho = \frac{R}{D},$$

and

$$f_{\text{SiO}_x} = \frac{L_{\text{so}}}{R + L_{\text{so}}} \left( 1 + \frac{2\pi \rho^2}{\sqrt{3}} \right), \quad (10)$$

$$f_{\text{SiO}_2} = 1 - f_{\text{c-Si}} - f_{\text{SiO}_x}.$$

In order to model the evolution of the interface during annealing, we use a power law to describe the reduction of both the protrusions (physical interface) and the chemical transition layer (chemical interface)

$$R = R^0 - \alpha(T_{\text{an}}) t_{\text{an}}^p,$$

and

$$L_{\text{so}} = L_{\text{so}}^0 - \beta(T_{\text{an}}) t_{\text{an}}^g, \quad (11)$$

where  $R^0$  and  $L_{\text{so}}^0$  are, respectively, initial values for the average radius of the protrusions and for the thickness of the chemical transition layer. The kinetic coefficients  $\alpha(T_{\text{an}})$  and  $\beta(T_{\text{an}})$  are annealing temperature dependent factors related to the rate limiting processes discussed below. The powers  $p$  and  $g$  are taken to be  $p = g = 0.5$  which is model dependent and justified below based on diffusion.

The minimization of the error function [Eq. (5)] for the sets of experimental data for the nonannealed wafer at  $\phi = 72^\circ$  and  $75^\circ$  with fitting parameters  $D$ ,  $R^0$ , and  $L_{\text{so}}^0$  (at  $x = 1$ ) gives the average distance between the centers of protrusions  $D = 44 \pm 4$  Å, initial radius of the protrusions  $R^0 = 9.8 \pm 0.3$  Å and initial thickness of suboxide SiO  $L_{\text{so}} = 3.4 \pm 0.2$  Å. These results are in agreement with the interface geometry sensitive TEM study of the SiO<sub>2</sub>-Si, which shows that distances between protrusions at nonan-

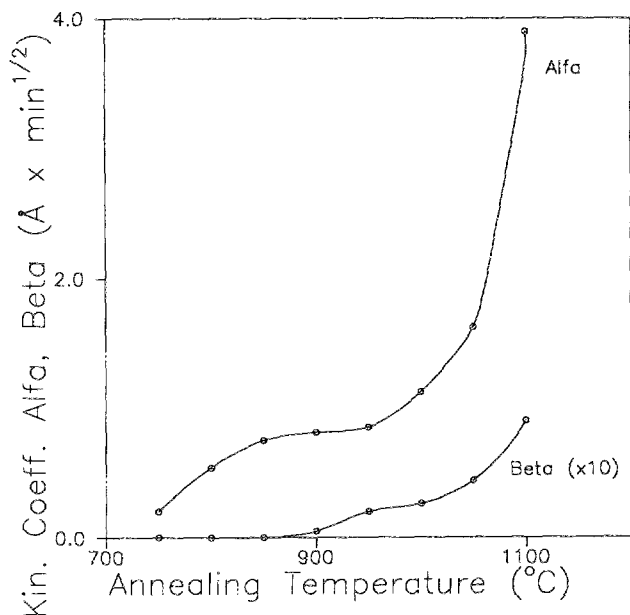


FIG. 5. The dependence of the kinetic coefficients  $\alpha$  and  $\beta$  on annealing temperature.

annealed interface are distributed in the range 40–50 Å and heights are 9–15 Å.<sup>1,2</sup> Also, photoelectron spectroscopy revealed a chemical transition layer with a thickness of 2.4–4 Å.<sup>11,32</sup>

The choice of  $x = 1$  for the composition  $\text{SiO}_x$  was made for several reasons. Virtually all the interface studies herein referenced as well as most others indicate that the interface region is Si-rich relative to  $\text{SiO}_2$ . Many of these studies indicate that  $x$  is near unity. The geometrical parameters  $D$ ,  $R$ , and  $L_{\text{so}}$  are correlated with  $x$ . Thus, by our fixing  $x$  at a known value, the determination of the other parameters is improved. We have calculated the variation in  $\epsilon_{\text{so}}$  with  $x$  from 0.8 to 1.2 at 3.2 eV (3.15–0.144i to 6.35–2.58i, respectively). This change is small relative to  $\epsilon_{\text{a-Si}}$  (19.47–24.6i) and comparable to  $\epsilon_{\text{SiO}_2}$  (2.2). Moreover the fraction of  $\text{SiO}_x$  in the transition layer is about 0.25 and the thickness of the suboxide layer is about 25% of the transition layer. Hence, a sensible variation of  $x$  around  $x = 1$  will result in less than 10% error in the geometrical parameters.

A simulation of the kinetic dependencies,  $\delta\Delta_{\text{inf}}(T_{\text{an}}, t_{\text{an}})$ , using Eqs. (7), (9)–(11) with  $p = g = 0.5$  yields the coefficients  $\alpha(T_{\text{an}})$  and  $\beta(T_{\text{an}})$  as functions of  $t_{\text{an}}$  or  $T_{\text{an}}$  as is shown in Fig. 5. At annealing temperatures less than 900 °C, the kinetic coefficient  $\beta(T_{\text{an}})$ , which characterizes the “chemical” interface evolution, is negligibly small and, therefore, the “chemical” interface is stable. The kinetic coefficient  $\alpha(T_{\text{an}})$  describing the “physical” interface evolution or the silicon protrusions diminution, is saturated and becomes temperature independent at  $T_{\text{an}}$  in the range of 850–950 °C. The comparison of the experimental plots of  $\delta\Delta_{\text{inf}}(t_{\text{an}})$  with simulations (dashed lines in Fig. 2) shows good agreement. Note, that the asymptotic form assumed for the interface reduction laws given as Eq. (11) (at  $t_{\text{an}} \gg 1$ ), is incorrect, since it leads to a disappear-

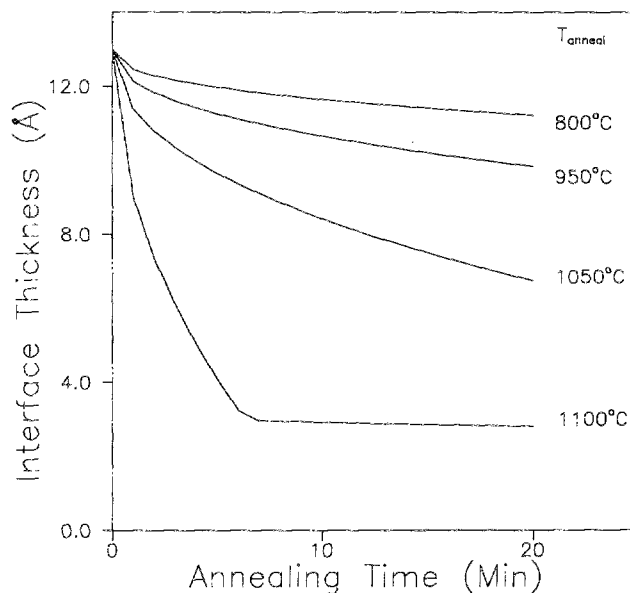


FIG. 6. The dependence of the effective interface thickness on annealing time at a number of annealing temperatures.

ance of the interface region after sufficient time of annealing. Nevertheless, the phenomenological model satisfactorily describes the experimental curves of Figs. 2 and 3 for tens of minutes and reflects the main features of the process.

Figure 6 displays the decrease of the extent of the interface,  $L_{\text{inf}}$ , i.e., effective thickness from Eq. (7) with a minimum thickness of about 3 Å realized at the highest anneal temperatures. The interface effective refractive index versus  $t_{\text{an}}$  at several  $T_{\text{an}}$  is shown in Fig. 7. Initially both the index and thickness of the interface layer decrease due to the shrinking of the silicon protrusions. This is followed by

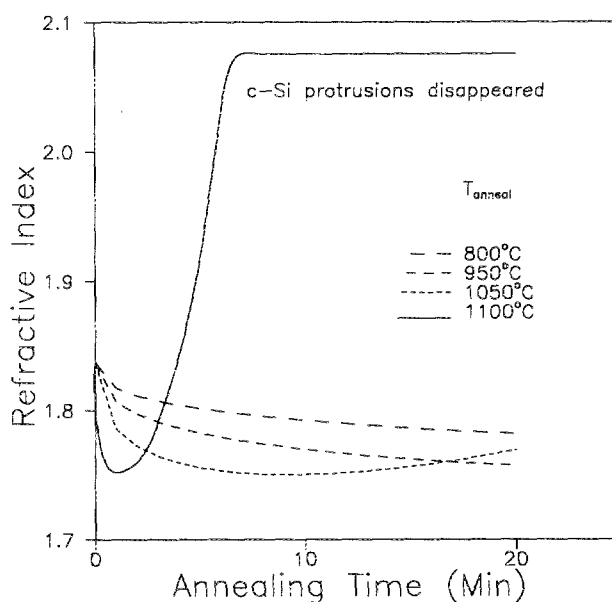


FIG. 7. The dependency of the effective interface refractive index on annealing time at a number of annealing temperatures.

the slower decrease of the SiO<sub>x</sub> transition layer which becomes dominant after considerable reduction of the height of the protrusions. The sharp increase in the index seen in Fig. 7 for the 1100 °C annealed sample is indicative of the index returning quickly to the SiO value as the fraction of the Si as protrusions in the interface layer rapidly goes to zero. The same effect would occur for the other anneal temperatures but more slowly. A slower rise in index is seen for the 1050 °C annealed sample after 10 min, and the time is too short to see the rise for the lower temperature anneals. The overall shape of the results in Fig. 7 is typical of and dictated by the BEMA model used to interpret the data.

#### IV. DISCUSSION OF THE INTERFACE MODEL

We have considered two interface regimes that decrease with annealing. The physical interface is typified by the Si protrusions that decrease in size and number during annealing. The driving force for this is the minimization of the interfacial free energy that requires an increase in the radius of curvature for interface protrusions or a reduction of the interface area covered by the protrusions with decreasing radius, thereby reducing the interface width. The chemical interface is typified by the suboxide and is reduced by the conversion of suboxide due to the presence of oxygen which produces SiO<sub>2</sub> or the evaporation of suboxide or to both, and by the relaxation of interfacial stress. The interfacial stress can also couple into the reduction of the physical interface by providing an additional driving force for the migration of atoms to reduce the protrusions. We discuss the viscous flow and interface reaction components of the interface annealing mechanism separately.

##### A. Viscous flow mechanism

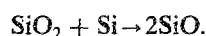
In the Si-SiO<sub>2</sub> system there is considerable evidence that stress relaxation occurs at high temperature by viscous flow<sup>22,24-25,33</sup> with a viscous flow point for bulk SiO<sub>2</sub> near 950 °C.<sup>23,24,30</sup> Stress relaxation by viscous flow decreases the oxide density with a relaxation time  $\tau$  expressed by Eq. (4). The characteristic relaxation time  $\tau$  is of the order of a few minutes at 1000 °C and a few hours at 900 °C.<sup>22-24,30</sup> This strongly suggests that the viscous flow mechanism may be dominant at temperatures higher than ~950 °C, but becomes negligible at lower temperatures and for annealing times less than ~1 h, i.e., the short annealing times of the present study. Furthermore, the temperature activated exponential nature of a viscous flow mechanism is not evident in Figs. 3 and 5 for temperatures below 950 °C, but is in evidence in these data at the higher anneal temperatures. From Fig. 3, we observe that at  $T_{an} < 900$  °C,  $\delta\Delta_{inf}(T_{an})$  (at constant time of annealing) tends to saturation, and the kinetic coefficients  $\alpha(T_{an})$  and  $\beta(T_{an})$  are saturated at  $T_{an} = 900-950$  °C (Fig. 5). Yet, at these lower temperatures significant change also occurs in the interface as evidenced in Figs 2 and 3. At high temperatures the migration of Si from the protrusions occurs via two driving forces: free-energy and stress. Another low temperature mechanism dictates the interface changes at low tempera-

tures, and we consider that the chemical reactions at the interface are likely important.

##### B. Interfacial chemical reaction mechanism

The reduction of both the physical and chemical interface can occur by the reduction in available Si at the interface. Above, the diffusion of Si atoms from the protrusions in response to the thermodynamic and mechanical forces was considered. However, it is difficult to understand how the chemical interface can be reduced by this mechanism, since Si from SiO<sub>2</sub> or SiO is not readily available to migrate.

Thermal dissociation of SiO<sub>2</sub> has received recent attention.<sup>34-36</sup> It was shown that at elevated temperatures and with an oxygen deficiency (vacuum or an inert gas ambient) the SiO<sub>2</sub> decomposition takes place via an interface reaction<sup>34</sup>



At temperatures  $T_{an} > \sim 900$  °C voids are formed at the interface after long-term vacuum annealing. The kinetics of the void growth<sup>34</sup> demonstrates that the oxide decomposition reaction is initiated at active defect sites already present at the Si/SiO<sub>2</sub> interface. Annealing at ~750-900 °C which is insufficient for void growth, transforms these defects into an electrically active state which seem to cause low-field dielectric breakdown.<sup>35,37</sup> The Si protrusions cannot be excluded from consideration as defects that could cause the above SiO<sub>2</sub> disproportionation, since these sites are thermodynamically active owing to the smaller radius of curvature. It is noteworthy that Walkup and Raider<sup>38</sup> did not observe the escape of SiO during defect formation and indeed the diffusion of SiO in SiO<sub>2</sub> would likely not be a favored process. However, if dissolved traces of oxygen or water are present, in the overlying SiO<sub>2</sub> and/or in the anneal ambient, this available oxidant might remove SiO through formation of SiO<sub>2</sub>. In our experiments, we have used pure anneal gases and careful procedures. However, our anneal systems are open flowing systems and our gases are from tanks. Thus trace amounts of oxidants are present and can be dissolved and accumulated in the SiO<sub>2</sub>. It was shown<sup>35</sup> that with sufficient O<sub>2</sub> (ppm level) present during inert gas annealing, O<sub>2</sub> reoxidizes SiO at the defects and prevents the low-field breakdown. This chemistry may lead to a gradual reduction of the active defect sites and causes the saturation of  $\delta\Delta_{inf}(T_{an}, t_{an})$  at  $T_{an} < 900$  °C seen in Fig. 3. From these data in the low temperature region it can be argued that a reduction both of O<sub>2</sub> concentration in the interface layer and the active sites due to oxidation could be rate-limiting factors.

In the anneal temperature region  $900$  °C  $< T_{an} < 970$  °C both mechanisms, viz. relaxation and chemical reaction are in evidence. We have assumed that the interfacial diffusion of atoms is a limiting process for the evolution of both the "physical" and the "chemical" interface. At high temperatures ( $T_{an} > 950$  °C), the "physical" interface changes by the diffusion of Si atoms away from protrusions and viscous flow of SiO<sub>x</sub> (or SiO<sub>2</sub>) in the opposite direction. At 1000 °C the viscous flow relaxation time is a few minutes,

but as seen in Fig. 2 the interface continues to change for longer times with a slower rate. After the fast and ample reduction of the extent of the physical interface for  $t_{\text{an}} < \sim 10$  min, the interface evolves slowly (with  $\beta \ll \alpha$ ) by the reduction of the chemical interface via the interfacial diffusion-limited reactions of decomposition and oxidation of suboxide. At moderate temperatures ( $T_{\text{an}} < 900^\circ\text{C}$ ), the decrease of SiO<sub>x</sub> ( $x \leq 2$ ) is diffusion limited<sup>39</sup> likely by the diffusion of oxidant through the silica network to the interface. Thus, it was reasonable to use a diffusional square-root time law for the "physical" and "chemical" interface evolution, i.e.,  $p = g = 0.5$ , and a good fit was found. According to the model developed here, annealing in an oxidant-free atmosphere at low temperatures, where the reoxidation reaction  $2\text{SiO} + \text{O}_2 \rightarrow 2\text{SiO}_2$  cannot take place will result in no annihilation of the electrically active sites.

## V. CONCLUSIONS

A novel enhanced interface sensitivity immersion spectroscopic ellipsometry technique was applied to study the Si/SiO<sub>2</sub> interface annealing. Two distinct stages of interface evolution were found. A fast initial stage with interface microroughness reduction followed by a slow decay of the interfacial suboxide. The interfacial suboxide reoxidation reaction dominates the interface evolution in the moderate temperatures region ( $T_{\text{an}} < 900^\circ\text{C}$ ) and viscous flow becomes dominant at elevated temperatures ( $T_{\text{an}} > 950^\circ\text{C}$ ).

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